

# A rotor wake – rotor tonal interaction noise computation procedure for contra-rotating fans

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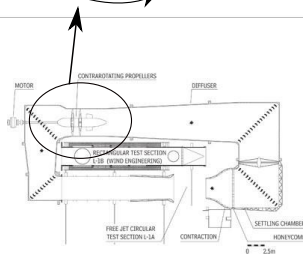
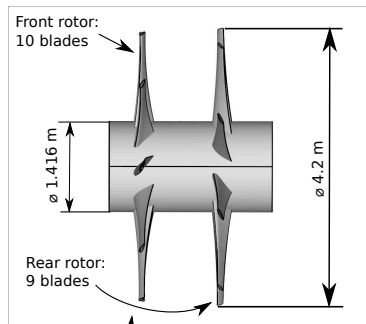
## 1 Introduction

## 2 Aeroacoustic theory and its application

- Tonal vs. broadband noise
- Synthetic wake generation
- Computation of the blade loading harmonics

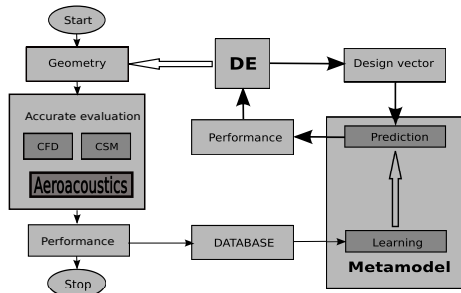


- CROR architectures are substantially more efficient than normal propellers, but a major drawback is the high noise emission.
- Development of an aeroacoustic evaluation procedure that can be implemented in the phase of preliminary design of a CROR.
- Application case: contra-rotating fans of VKI-L1 wind tunnel.



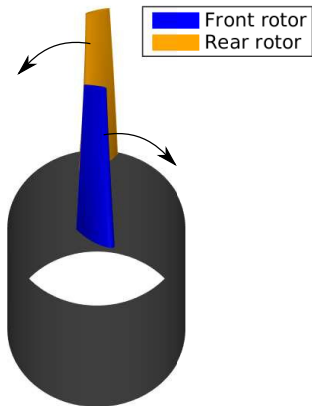
# Introduction

- An aerodynamic - aeroacoustic optimization of this geometry has been performed.
- In-house optimization software: CADO.
- Simplified noise evaluation method.
- The results of this optimization will now be analysed in the light of a more advanced noise computation algorithm.

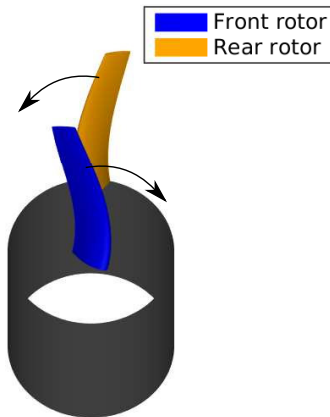


# Geometric configurations of interest - effect of lean and sweep

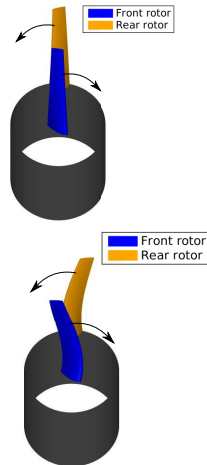
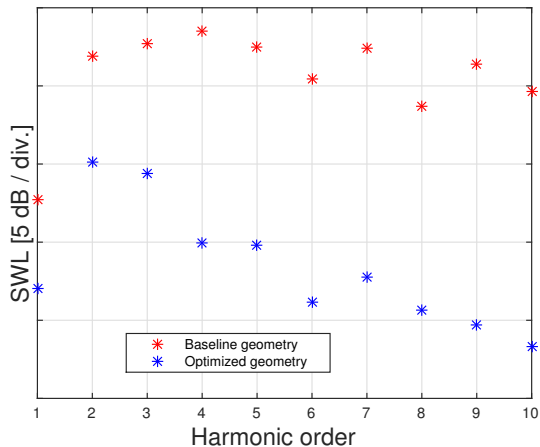
Baseline geometry



Optimized geometry



# Far-field tonal noise spectrum



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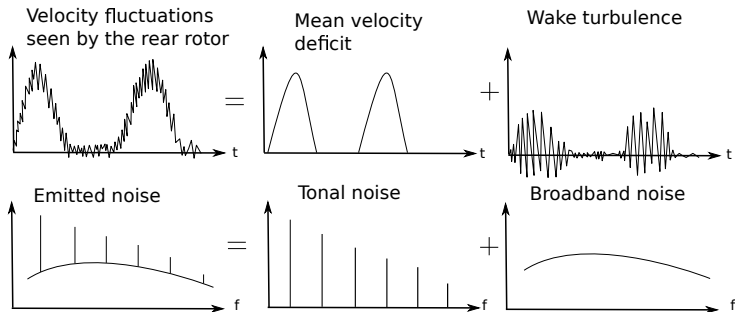
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# Linearised aeroacoustic theory



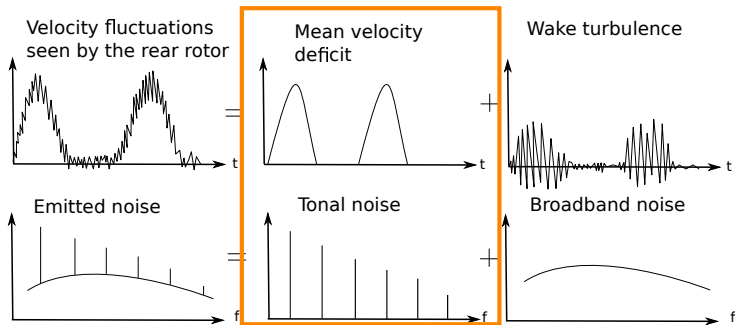
Decoupling of the aeroacoustic phenomena related to wake interaction:

- mean velocity variation in the wake causes tonal noise;
- wake turbulence causes broadband noise.

(Fournier, 1988)



# Linearised aeroacoustic theory



Decoupling of the aeroacoustic phenomena related to wake interaction:

- mean velocity variation in the wake causes tonal noise;
- wake turbulence causes broadband noise.

(Fournier, 1988)



# Ffowcs Williams and Hawkings analogy

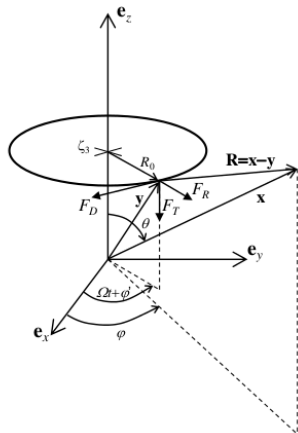
Sound pressure emitted at a given harmonic  
of the BPF of the rear rotor (Goldstein,  
1976):

$$p'_{nB} \sim -\frac{iBk_{nB}}{4\pi} \frac{e^{-ik_{nB}x}}{x} \sum_{p=-\infty}^{+\infty} e^{-i(nB-p)(\phi-\phi_0-\pi/2)} \dots$$

$$\begin{aligned} & \left( J_{-nB+p}(-k_{nB}R_0 \sin \theta) F_p^{(T)} \cos \theta \dots \right. \\ & - \frac{nB-p}{k_{nB}R_0} J_{-nB+p}(-k_{nB}R_0 \sin \theta) F_p^{(D)} \dots \\ & \left. - iJ'_{-nB+p}(-k_{nB}R_0 \sin \theta) \sin \theta F_p^{(R)} \right). \end{aligned}$$

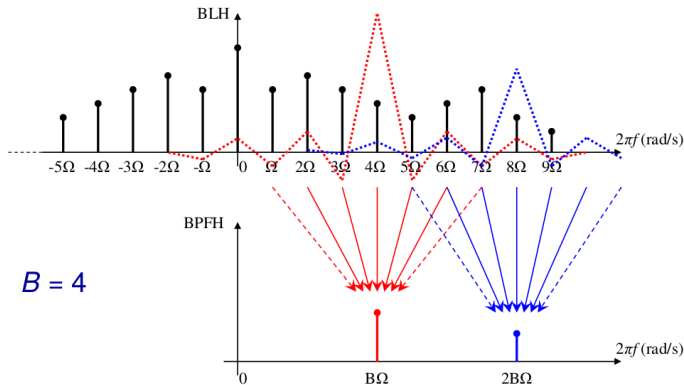
$x, \phi, \theta$ : spherical coordinates of the listener position.

$\phi_0$ : relative azimuthal displacement of the source locations  $\rightarrow$  retarded time effect.



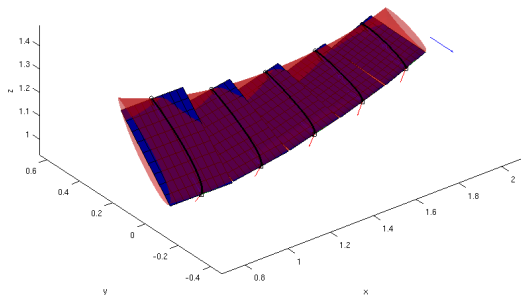
# Ffowcs Williams and Hawkings analogy

Bessel functions modulate the Doppler frequency shift during blade revolution.



# Approximation of the blade geometry with rectangular strips

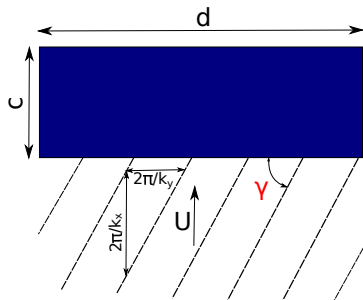
- Amiet's theory approximates slightly cambered airfoils with flat plates.
- Dividing the blade in rectangular strips allows to take into account spanwise variation of flow conditions.
- The overall noise is the sum of the noise emitted by each strip.



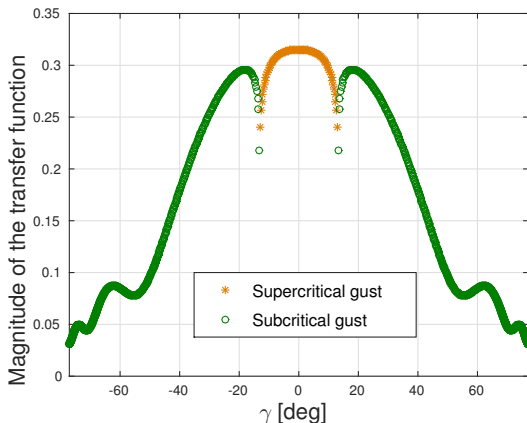
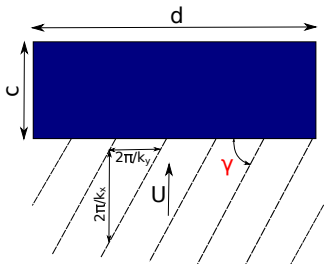
# Formulation of the unsteady lift

$$L(k_x, k_y) = 2 \pi \rho_0 U (c/2) \hat{\hat{w}}(k_x, k_y) G(c_0, (c/2), k_x, k_y, U) \dots \\ i (\exp(-i k_y d/2) - \exp(i k_y d/2)) / k_y$$

$\hat{\hat{w}}(\mathbf{k}_x, \mathbf{k}_y)$  is the double spatial Fourier transform of the velocity disturbance.  
 $\mathbf{G}$  is the aerodynamic transfer function from the velocity disturbance to the unsteady lift.  
(Amiet, 1975)



# Effect of $\gamma$ on the transfer function computation



The magnitude of the response function can be reduced to less than a third by increasing the skewness of the wake.



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# Synthetic wake generation

## General equations

Mathematical model based on the empirical correlations of Raj and Lakshminarayana (1976).

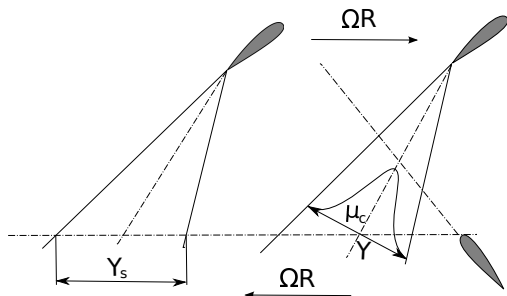
Decaying of the defect in mean velocity at the wake centerline:

$$\frac{\mu_c}{U} = \exp \left[ - \frac{\pi^2}{14} \left( \frac{s}{S'} + 3.46 \right) \right]$$

being  $s$  the streamwise direction and  $S'$  the blade spacing (projected).

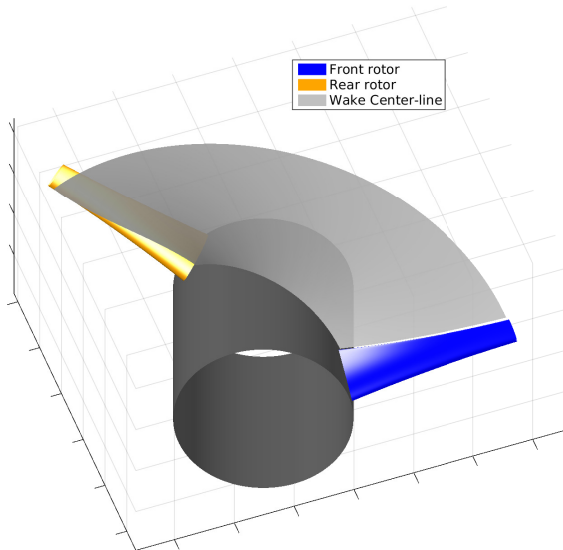
Wake width variation:

$$\frac{Y_s}{Y_{s0}} = 1.61 \left( \frac{s}{S'} \right)^{0.23}$$



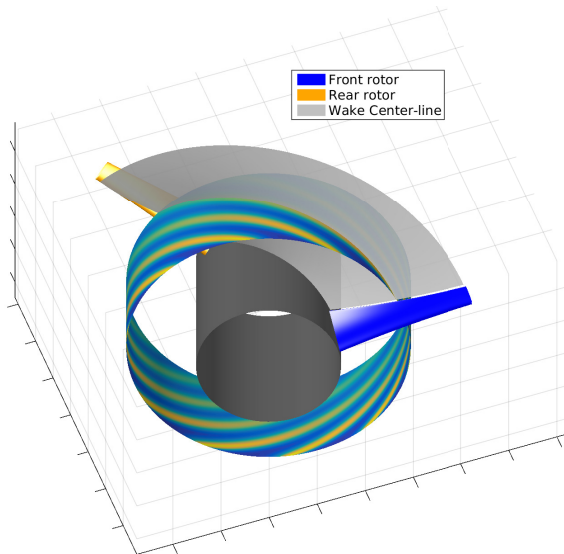
# Synthetic wake generation

Application to baseline configuration



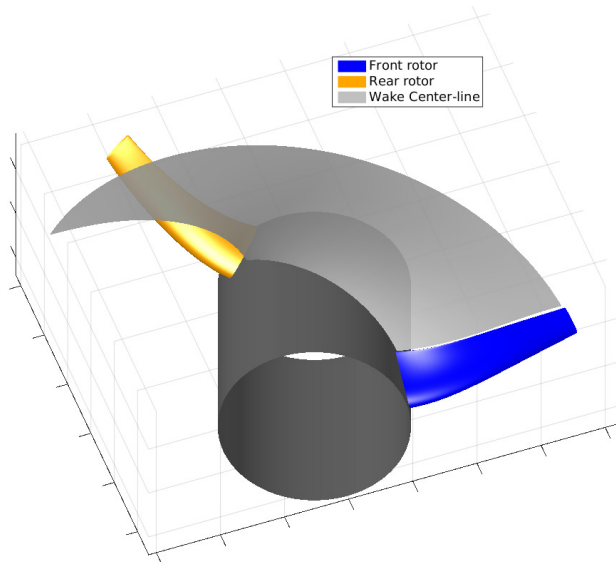
# Synthetic wake generation

## Application to baseline configuration



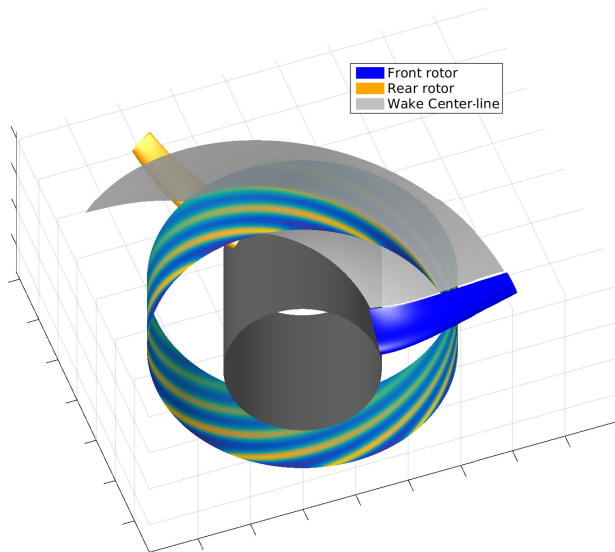
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Application to optimized configuration



# Synthetic wake generation

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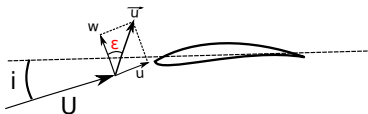
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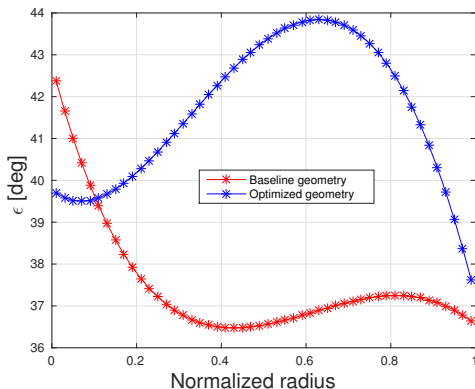
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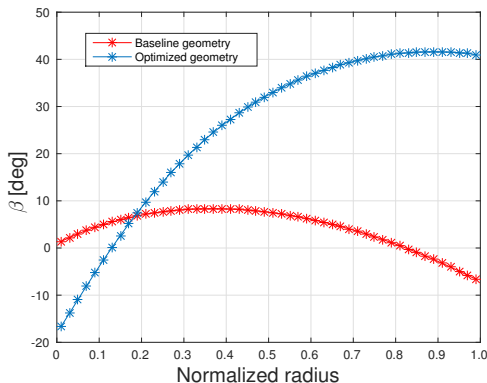
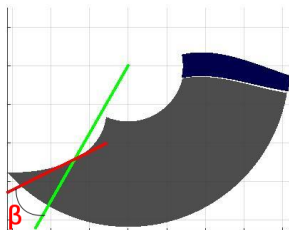
# Projection of the upwash component of the velocity disturbance



The upwash component of the velocity disturbance is responsible for the major part of the unsteady lift.



# Inclination of the wake center-line in the secondary plane

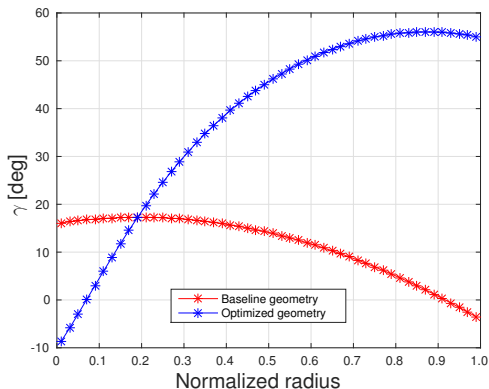
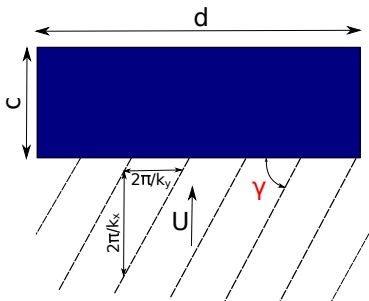


$\beta$  is invariant with the rotation of the wake. Its computation is necessary to project the wake in the frame of reference attached to each rear blade strip.





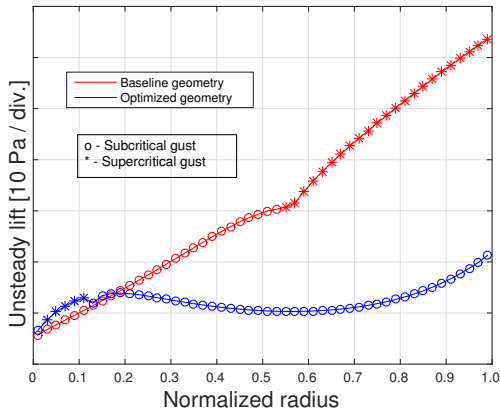
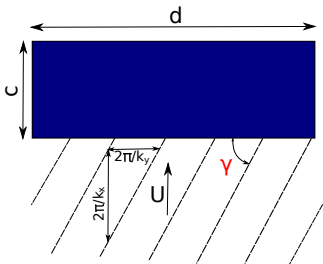
# Inclination of the incoming gust, $\gamma$



The incoming wake is projected, at every radial position, in the plane of the rear rotor strip.



# Computation of the unsteady lift - dipolar source of noise



First BLH magnitude.



# Conclusions and future work

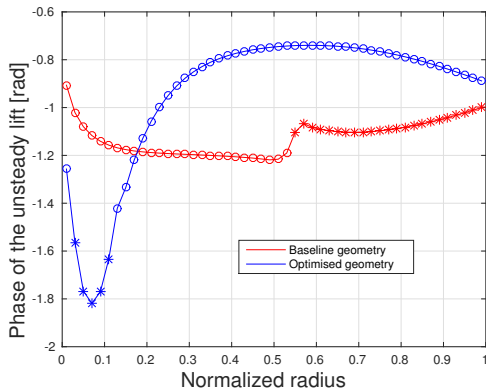
- The synthetic wake generation algorithm has been useful to understand the geometric parameters that influence the wake-blade interaction.
- The skewness of the wake seen by the rear rotor is the key parameter that can reduce the blade loading harmonics and thus the emitted noise.
- Secondary flow phenomena have not been taken into account. The noise computation will be based on CFD data. RANS simulations will be used to reduce computational cost (implementation of a wake extrapolation procedure).
- Modelling of broadband noise related to incoming turbulence.



Thank you for your kind attention.  
Any question?

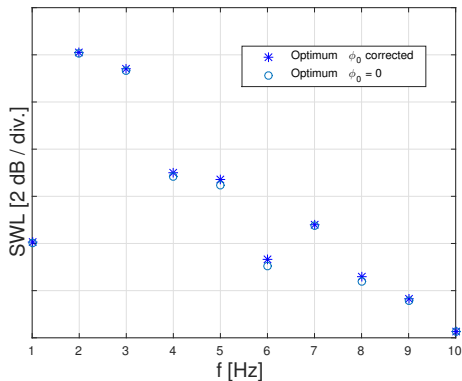


# Retarded time effects in the wake-rotor interaction



# Retarded time effects in the propagation of noise

## Optimized configuration



- G. Grasso, J. Christophe, C. Schram, T. Verstraete, *Aerodynamic, aeroacoustic and structural optimization of a contra-rotating Fan*, 15th International Symposium on Transport Phenomena and Dynamics of Rotating Machinery, ISROMAC-15, Honolulu, USA, 2014.
- G. Grasso, J. Christophe, C. Schram, T. Verstraete, *Influence of the noise prediction model on the aeroacoustic optimization of a contra-rotating fan*, 20th AIAA CEAS Aeroacoustics Conference, Atlanta, USA, 2014.
- G. Grasso, J. Christophe, C. Schram, *Numerical performance and accuracy of wake interaction noise prediction models*, International Conference on Noise and Vibration Engineering, Leuven, BE, 2014.
- G. Grasso, J. Christophe, C. Schram, *Broadband trailing-edge noise prediction of a four-bladed axial fan*, International Conference on Fan Noise, Technology and Numerical Methods, Lyon, FR, 2015.

